## 50 Years of Research in ARDS

# **Tidal Volume Selection in the Acute Respiratory Distress Syndrome**

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Abstract

Mechanical ventilation (MV) is critical in the management of many patients with the acute respiratory

distress syndrome (ARDS). However, MV can also cause ventilator-induced lung injury (VILI). The

selection of an appropriate tidal volume is an essential part of a lung-protective MV strategy. Since the

publication of a large randomized clinical trial demonstrating the benefit of lower tidal volumes, the use

of tidal volumes of 6 mL/kg predicted body weight (PBW, based on sex and height) has been

recommended in clinical practice guidelines. However, the PBW approach is imperfect in ARDS patients

because the amount of aerated lung varies considerably due to differences in inflammation,

consolidation, flooding, and atelectasis. Better approaches to setting tidal volume may include limits on

end-inspiratory transpulmonary pressure, lung strain, and driving pressure. The limits of lowering tidal

volume have not yet been established, and some patients may benefit from tidal volumes that are lower

than those in current use. However, lowering tidal volumes may result in respiratory acidosis. Tactics to

reduce respiratory acidosis include reductions in ventilation circuit dead space, increases in respiratory

rate, higher positive end-expiratory pressures (PEEP) in patients who recruit lung in response to PEEP,

recruitment maneuvers, and prone positioning. Mechanical adjuncts such as extracorporeal carbon

dioxide removal may be useful to normalize pH and carbon dioxide levels, but further studies will be

necessary to demonstrate benefit with this technology.

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#### Introduction

Mechanical ventilation (MV) is critical for survival of many patients with the acute respiratory distress syndrome (ARDS). However, MV can also cause ventilation-induced lung injury (VILI), which can exacerbate or perpetuate injury from the original cause of ARDS, such pneumonia, sepsis, or trauma.(1-5) One mechanism of VILI is overdistention of aerated lung tissue.(6) ARDS patients are especially vulnerable to this because the volume of aerated lung available for ventilation is reduced, greatly in some patients. Therefore, a tidal volume ( $V_T$ ) that might be gentle and harmless in a normal subject may cause serious injury from overdistention in ARDS patients. To prevent or reduce VILI from overdistention, we usually use  $V_T$ s that are substantially smaller than those that were used in the past, before the potential for VILI from overdistention was recognized.(7, 8)

Setting  $V_T$  is an important part of MV management of ARDS patients. Several approaches for adjusting  $V_T$  to prevent VILI have been suggested. In this review we explain the rationale behind different methods, review data that support them, and comment on certain practical aspects of setting  $V_T$  for ARDS patients. This discussion is written with the assumption that the ventilator mode allows direct control over  $V_T$ , as with the Volume-Assist/Control mode, or indirect control as with Pressure-Assist/Control mode in patients who are not making respiratory efforts. Moreover, additional considerations are needed when patients are making spontaneous inspiratory efforts even when on controlled modes of ventilation. The risks and management of spontaneous breathing during mechanical ventilation has been expertly reviewed recently.(9)

#### **Volume Control versus Pressure Control Modes**

In Volume-Assist/Control modes, depending on the patient's respiratory system compliance, the resulting inspiratory alveolar pressure may be low, intermediate, or high. If it is too high, the clinician may reduce the set  $V_T$ . With a mode that allows direct control of the pressure during inspiration, as with the Pressure Control mode, the  $V_T$  that results from the inspiratory pressure increment depends on the

magnitude and duration of the increment and a patient's respiratory system compliance (lung and chest wall combined) and airway resistance. The pressure control increment and duration can be adjusted if the initial  $V_T$  is not at the desired volume. Some modes, such as Pressure Regulated Volume Control and AutoFlow, allow control over the  $V_T$  if the patient has no respiratory efforts. However, control over  $V_T$  is lost in these modes when patients begin to make spontaneous respiratory efforts.(9)

Pressure and volume are inextricably entwined according to each patient's respiratory system pressure-volume relationship. Therefore, theoretically we can achieve the same tidal volume and airway pressure pattern of ventilation with either mode. The choice of modes is usually dictated by clinicians' experiences and preferences. Some prefer the pressure control mode because they can set the pressure during inspiration to a level that they think is safe. This may have some merit when patients are passive, not making any efforts to breath. However, if patients make inspiratory efforts in the pressure control mode, the resulting V<sub>T</sub>s can be large even though the airway pressure is not high, causing substantial overdistention.(10, 11) Thus, one advantage of the volume control modes is that we have better control over V<sub>T</sub>s. A disadvantage of the volume control mode is that the inspiratory flow is preset. In patients who have a high inspiratory drive, the flow setting may result in frequent double-breaths, which can cause VILI from overdistention. (Figure 1) Nevertheless, although the volume and pressure control modes are very different, current data do not show any difference in clinical outcomes between the modes.(11)

#### **Methods for Setting Tidal Volume**

#### Setting Tidal Volume According to Body Weight

A historical approach set  $V_T$ s according to actual body weight. Larger patients generally have larger lungs, so patients with larger lungs would usually receive larger  $V_T$ s. In a comprehensive review of acute respiratory failure in adults from 1972, the authors recommended generous  $V_T$ s of 10 to 15 mL/kg.(7) There were two problems with this recommendation. First, although lung size correlates with body

weight, body weight varies substantially between patients because of differences in adipose tissue, muscle mass, and extravascular fluid, independent of lung size. Second, these large  $V_T$ s would tend to cause VILI from overdistention in patients at risk for or with established ARDS.

Four randomized clinical trials of traditional, generous  $V_T s$  vs lower  $V_T s$  in patients with or at risk for ARDS used estimations of lean body weight to set tidal volumes.(12-15) One trial used an equation for "ideal body weight" that did not account for variations in lung size according to sex.(13) Two of the trials used equations for "predicted body weight" (PBW) that accounted for both sex and height: (14, 15)

Female PBW (kg) = 
$$45.5 + 0.91$$
(cm of height –  $152.4$ )

Male PBW (kg) = 
$$50 + 0.91$$
 (cm of height –  $152.4$ )

Several subsequent clinical studies and randomized trials used PBW to set tidal volumes (16-20), and some clinical guidelines recommended this approach.(21, 22)

According to the National Institutes of Health ARDS Network protocol, the goal for  $V_T$ s is 6 mL/kg PBW, with an inspiratory plateau pressure (Pplat) limit of 30 cm  $H_2O$ . If the Pplat exceeds 30 cm  $H_2O$  on a  $V_T$  of 6 mL/kg PBW, the protocol recommends a reduction in  $V_T$  to 5 or 4 mL/kg PBW if arterial pH is > 7.15. The goal of 6 mL/kg PBW was chosen to be lung-protective without causing severe respiratory acidosis in most patients. The ARDS Network trial demonstrated improved clinical outcomes with a  $V_T$  goal of 6 mL/kg PBW as opposed to a  $V_T$  goal of 12 mL/kg PBW. Some investigators suggested that it is not necessary to reduce  $V_T$ s if the Pplat is < 30 or 32 cm  $H_2O$ .(23, 24) However, an analysis of the ARDS Network  $V_T$  trial suggested that there were beneficial effects of  $V_T$  reduction even among patients whose Pplats would have been  $\leq$  26 cm  $H_2O$  if they received  $V_T$ s of 12 mL/kg PBW.(25) Two other studies suggested that Pplats in the mid-20s were safer than Pplats in the high-20s.(20, 26)

A shortcoming of the PBW approach is that the volume of aerated lung varies substantially among ARDS patients because, at a given gender and height, there is a substantial variability in normal lung volumes.(27) Moreover, among ARDS patients, there are large differences in the extent of the lung inflammation, edema, atelectasis, and consolidation. These are the main reasons why, at a given V<sub>T</sub>, Pplats vary greatly among ARDS patients of the same sex and height. The Pplat limit of 30 cm H<sub>2</sub>O leads to additional reductions in V<sub>T</sub> in patients with more extensive disease. However, in some patients, high inspiratory pressures are caused by high chest wall elastance and weight rather than extensive lung disease.(28, 29) A better approach could be to set V<sub>T</sub> according to some objective measure of aerated lung volume, such as the functional residual capacity.(30, 31)

### Setting V<sub>T</sub> to Reduce Driving Pressure

Driving pressure (DP) is easily calculated at the bedside as the difference between the airway inspiratory plateau pressure and the PEEP (DP = Pplat - PEEP). It is determined by the ratio of the tidal volume to the compliance of the respiratory system (DP =  $V_T/C_{RS}$ ). Because  $C_{RS}$  is directly related to the size of the lung participating in ventilation, driving pressure reflects the size of the  $V_T$  in relation to the aerated lung volume. Assuming no auto-PEEP, DP estimates the average increase in alveolar pressure during inspiration and decrease during exhalation. Unlike Pplat and PEEP, which are static estimates of stress in the respiratory system, DP is a dynamic indicator, the *change* in stress with each breath. An individual patient data meta-analysis of predictors of mortality included over 3,000 ARDS patients enrolled in clinical trials of lung-protective ventilation strategies.(32) All patients in the meta-analysis were ventilated with a PEEP of at least 5 cm  $H_2O$ . DP was the strongest predictor of mortality among the mechanical ventilation variables that clinicians can manipulate (tidal volume, Pplat, PEEP, respiratory rate). At a constant DP, variations in tidal volume, PEEP, and Pplat did not predict mortality. The median DP was approximately 14 cm  $H_2O$ , and the relationship of mortality to DP appeared to increase more steeply above 14 cm  $H_2O$ . (Figure 2) This might suggest that we should reduce  $V_T$  until DP is below 14 cm

 $H_2O$ . When DP is less than 14 cm  $H_2O$  with  $V_T$  greater than 6 mL/kg PBW, the value of further  $V_T$  reduction is likely less, as other factors may take on more importance. The magnitude of the effect of DP on mortality in this meta-analysis may be partly attributable to the higher range of DPs included from the studies examining higher versus lower  $V_T$ .(33) In the  $V_T$  trials, DP ranged from approximately 10-15 cm  $H_2O$  in the low tidal volume group and approximately 20-25 cm  $H_2O$  in the control group. Subsequent mechanical ventilation trials on higher versus lower PEEP levels limited  $V_T$  to 6 mL/kg PBW, and DP ranged from 12-17 cm  $H_2O$  in both control and intervention groups. However, in the patient data meta-analysis, the mortality rate among patients with DP below 14 cm  $H_2O$  was still approximately 20%. Further, the slope of the relationship between DP and mortality appears to be positive even at DP below 14 cm  $H_2O$ , suggesting that there is no safe upper limit for DP in ARDS patients on positive pressure ventilation.

Another problem with using DP to set  $V_T$  is that Pplat, one of the components of DP, is influenced by the chest wall. Two patients with the same DP might have very different risks for VILI. At a given DP, a patient with a stiff or heavy chest wall likely has less overdistention of the lung than a patient with a normal chest wall. Therefore, a better indicator of dynamic stress in the lung would be the transpulmonary driving pressure (DP-P<sub>L</sub>), which is the difference in transpulmonary pressure ( $P_L$  = airway pressure minus pleural pressure) between end-expiration to end-inspiration.(34) However, there are several assumptions and potential limitations of measuring PL, and we do not know the safe upper limit for DP-P<sub>L</sub>.(35) This probably varies depending on the severity of the lung injury from pneumonia, sepsis, or whatever the inciting cause of ARDS.

## Setting V<sub>T</sub> to Reduce Lung Stress

The stress of an object is the force applied to it divided by its surface area. In the lungs, a static  $P_L$  represents the stress in the lungs at a given lung volume. (34) At the end of inspiration,  $P_L$  represents the highest level of stress during the respiratory cycle, which is determined by the positive end-expiratory

pressure (PEEP) and the size of the  $V_T$  relative to the amount of aerated lung. Thus,  $P_L$  may be used as a marker of potential overdistention injury, and  $V_T$  could be limited to maintain end-inspiratory  $P_L$  below a critical limit. A previous investigation suggested a critical limit of 27 cm  $H_2O$  for end-inspiratory  $P_L$  in humans.(36) Other models, however, have proposed much lower limits for acceptable lung stress during inspiration. Using a theoretical model, Gattinoni and colleagues suggested the limit to avoid overdistention was an end-inspiratory  $P_L$  of 15 cm  $H_2O$ , which corresponds to approximately 70 to 75% of total lung capacity in normal humans.(37) In healthy pigs ventilator-induced pulmonary edema occurred at an average inspiratory  $P_L$  of 13 cm  $H_2O$ .(38)

At this time, the only method for estimating pleural pressure in patients is esophageal manometry, and several questionable assumptions are required when we use this technique. (35) Furthermore, there are different methods of calculating  $P_L$ , which yield results that sometimes differ substantially based on which calculation is used. (39) At this time, there do not appear to be clear boundaries for  $P_L$  in humans. In the future, clinicians will need reliable measurements for  $P_L$  and reliable targets for safe limits of stress before this measure can be used to optimize  $V_T$ s.

## Setting V<sub>T</sub> to Reduce Strain

Strain is the ratio of the stretch of an object to its resting length. In the lung, strain at end-inspiration can be represented by the  $V_T$  normalized to the functional residual capacity (FRC) measured at an airway opening pressure of 0 cm  $H_2O$ . Lung strain is directly related to stress through the specific lung elastance and, like stress, may be utilized as a marker of overdistention.(36) Similar to lung stress, the strain resulting from a given  $V_T$  varies substantially among ARDS patients because of variations in aerated lung volume at FRC. (36) In a study by Chiumello and colleagues, the same measured strain and stress could be generated with both low tidal volumes of 6 mL/kg PBW and high tidal volumes of 12 mL/kg within subgroups of patients that included some without lung disease and some with ARDS, further demonstrating the inadequacy of Pplat and  $V_T$  per PBW for predicting overdistention injury.

VILI related to excessive strain may be related to both its dynamic and static components. Static strain results from the application of PEEP, which causes an isotonic deformation of the aerated lung above FRC at end-expiration. Dynamic strain results from the cyclic inflation of aerated lung with each tidal breath. Protti and colleagues demonstrated in healthy pigs that ventilator-induced pulmonary edema developed only when  $V_{\tau}s$  resulted in dynamic lung strains greater than 1.5-2.0. (38) In further investigations, lung injury was primarily related to dynamic strain rather than static strain. At the same peak inspiratory strain, ventilation with smaller dynamic and larger static strains were associated with less lung injury compared to ventilation with smaller static and larger dynamic strains. (40)

An individualized setting of  $V_T$  based on reducing dynamic strain would be a more direct method to reduce stretch-induced lung injury than setting  $V_T$  according to PBW. This method, however, requires a valid measurement of FRC, which can be difficult in critically ill patients. Values of FRC can be measured by gas dilution, nitrogen wash-in/wash-out, and quantitative CT analysis. Unfortunately, these methods are relatively complex, cumbersome, or risky, which has limited the clinical implementation of these techniques.

Another limitation to using strain to set  $V_T$  is that in many ARDS patients, recruitment of lung tissue occurs during inspiration. When this occurs the ratio of  $V_T$ /FRC overestimates the strain in the aerated lung parenchyma because some of the  $V_T$  is distributed to some alveoli that open during inspiration rather than stretching of previously aerated alveoli. To reduce this error, strain could be assessed from the ratio of  $V_T$  to Total Lung Capacity (TLC).(41) A challenge to this approach is to define TLC in an ARDS patient. Another challenge is that we do not know a safe upper limit of strain measured with this approach.

There is increasing interest in electrical impedance tomography for monitoring regional changes in lung volume at the bedside. EIT may be useful for monitoring regional compliance and to assess changes in

end-expiratory lung volume during PEEP titration. It is unclear if the regional assessment of volume change is an adequate surrogate for global volume change. However, it is non-invasive, relatively easy to implement, and may be helpful in adjusting  $V_T$ . As research utilizing EIT continues to grow, its use in the clinical setting may also expand.(42)

## Preventing or Reducing Hypercapnia and Acidosis When Using Small V<sub>T</sub>

Smaller V<sub>T</sub> may lead to respiratory acidosis, especially in patients with high physiologic dead space, as in ARDS. Some ventilator circuits contain unnecessary dead space. Endotracheal tube extenders and heat and moisture exchangers (HME) are attached to the tip of the endotracheal tube and fill with alveolar gas at end-expiration. This CO<sub>2</sub>-laden gas is then delivered back into the lungs with the next inspiration. Some HMEs contain as much as 80 mL of volume, which converts otherwise effective alveolar ventilation into dead space. Heated humidifiers are more effective for conditioning inspired air and, because of their location in the ventilator circuit, do not impose additional dead space. Additionally, endotracheal tube extenders can be removed from the circuit to reduce instrumental dead space. A simple approach to reducing hypercapnia and respiratory acidosis is to increase the respiratory rate. This technique was used in the ARDS Network lower tidal volume protocol, in which levels of respiratory acidosis on average were quite mild. Recruiting lung can also improve CO<sub>2</sub> clearance.(43) The use of higher levels of PEEP and recruitment maneuvers may help to reduce hypercapnia and acidosis in patients who respond with recruitment, by reducing physiologic dead space and shunt. (43) In those who do not recruit, higher PEEP can worsen dead space. (44) Prone positioning may lead to substantial recruitment in many ARDS patients, which may also reduce dead space and respiratory acidosis.

Additionally, increasing the duration of inspiration, as with an end-inspiratory pause, can decrease

PaCO<sub>2</sub> in small amounts to decrease acidosis from smaller V<sub>T</sub>s.(45, 46)

Mechanical adjuncts such as extracorporeal carbon dioxide removal (ECCO<sub>2</sub>R) may facilitate the use of very low tidal volumes by mitigating hypercapnia. Recent trials have demonstrated the feasibility of an ultra-protective ventilation strategy with concomitant use of low flow veno-venous ECCO<sub>2</sub>R to reduce respiratory acidosis. (47, 48) In 15 patients,  $V_T$  was reduced to approximately 4 mL/kg PBW, and ECCO<sub>2</sub>R was effective for preventing severe respiratory acidosis. Six of the patients, however, experienced persistent hypoxemia and required either prone positioning or extracorporeal membrane oxygenation (ECMO). This unanticipated hypoxemia may be a consequence of lower airway pressures causing increased atelectasis.(49) These effects may be counteracted by periodic recruitment maneuvers or higher levels of PEEP. In the second trial, 79 patients were randomized to  $V_T$  of 3 mL/kg PBW combined with ECCO<sub>2</sub>R or to a control group with  $V_T$  of 6 mL/kg PBW. Patients with a PaO<sub>2</sub>/FiO<sub>2</sub>  $\leq$  150 demonstrated significantly improved ventilator-free days after 60 days in the ECCO<sub>2</sub>R study group, although overall mortality rate did not differ between the two groups.(48) More investigation is warranted before fully embracing this technologic adjunct. A multicenter randomized clinical trial is currently enrolling to test the feasibility, safety, and efficacy of using ECCO<sub>2</sub>R to enable ultra-protective ventilation. (SUPERNOVA Clinicaltrials.gov NCT02282657).

High-frequency Oscillatory Ventilation (HFOV) delivers small  $V_T$ s of approximately 1-3 mL/kg PBW at very high respiratory rates. (50) These very small tidal volumes limit overdistention while relatively high mean airway pressures prevent cyclic alveolar collapse and reopening. (51) An early randomized clinical trial of HFOV versus conventional MV in ARDS demonstrated a trend towards lower mortality with HFOV. However the conventional MV group utilized generous  $V_T$ s of greater than 10 mL/kg PBW, which are now known to be injurious. (52) More recent, larger randomized trials demonstrated either no difference in mortality or possible harm with HFOV compared to conventional MV with lower tidal volumes. (18, 19) Each of the HFOV trials were challenged by limitations in their design, which may have led to the HFOV groups receiving more sedation, fluids, vasopressors, and neuromuscular blocking agents. In the

absence of convincing evidence of efficacy, the use of HFOV is now largely limited to patients who have failed other rescue therapies or who are not candidates for mechanical support such as extra-corporeal gas exchange.

### Lower V<sub>T</sub> Reduces VILI Even at Lower Expiratory Pressures and Volumes

VILI may also occur from ventilation with low end-expiratory volume and pressure, perhaps from repeated opening and re-closing of small bronchioles and alveoli and from excessive stress at the margins between aerated and atelectatic or consolidated lung tissue.(5, 53) This form of VILI may be reduced with higher levels of PEEP than were used in the past, before VILI was recognized.(5, 53) However, recruitment and derecruitment occur at almost all lung volumes in ARDS patients, even when relatively high levels of PEEP are used.(54, 55) Regardless of the volume at end-expiration, the recruiting and derecruiting pressure swings are smaller when low V<sub>T</sub>s are used. Therefore, in addition to reducing VILI from overdistention, lower V<sub>T</sub>s can also reduce VILI from opening and reclosing or from excessive stress at the margins between aerated and atelectatic air spaces.(56, 57) Ultimately, the mechanical power that is applied to the lung decreases exponentially with reductions in V<sub>T</sub>, which may be a powerful mechanism for reducing VILI.(58)

## **Rethinking Goals for Setting Tidal Volume**

Several studies strongly suggest that in patients with ARDS, VILI from overdistention can occur at  $V_T$ s and Pplats that are lower than those that are in current use in most intensive care units.(20, 25, 26) Unfortunately, there is no reliable test for ongoing VILI from overdistention, like troponin for ongoing cardiac injury. Moreover, despite current guidelines and recommendations for  $V_T$ , Pplat, stress, strain, and DP, we do not know safe levels of any of these parameters. Therefore, we propose that any of the methods for setting  $V_T$  reviewed here can be used to set the *initial*  $V_T$ . We advocate that the initial  $V_T$  should be within the range of 4-8 mL/kg PBW with Pplat < 30 cm H<sub>2</sub>O. The upper part of this range, 7-8

mL/kg, should be reserved for patients who have frequent double breaths or severe dyspnea with airway pressure less than PEEP for much of the inspiratory cycle In patients with moderate and severe ARDS, and especially in patients whose DPs and plateau pressures are not comfortably low (DP > 14 cm  $H_2O$  and Pplat > 25 cm  $H_2O$ , respectively), we suggest that clinicians push the limits of reducing  $V_T$ beyond their current practice, setting  $V_T$ s in the lower part of our range of 4-6 mL/kg.  $V_T$  can be reduced in small decrements e.g. 0.5 mL/kg PBW) over several hours while monitoring individual patients' responses for signs of intolerance to the adverse effects of lower  $V_T$ s, including hemodynamic changes, gas exchange, and respiratory mechanics. (Table 1) In some patients, the ultimate V<sub>T</sub> may be considerably lower than those that are in common use today. (59) Furthermore, regardless of the method to set the initial  $V_T$ , if the same signs of intolerance are used, the same ultimate  $V_T$  will be attained. A shortcoming of this approach is that the signs of intolerance are not very specific to intolerance to hypercapnia and acidosis. However, if we monitor these signs closely over a period of a few hours while lowering  $V_T$  in steps, changes in these signs should more specifically represent effects of the lower V<sub>T</sub> implementation. If signs of intolerance develop, adjunctive therapies, such as neuromuscular blockade or ECCO<sub>2</sub>R, should be considered to facilitate tolerance of low V<sub>T</sub>, especially for patients who would likely benefit the most from reduced V<sub>T</sub>

#### **Conclusions**

The optimal method for setting  $V_T$  for ARDS patients remains unknown. The use of smaller  $V_T$ s has been accepted by many since the publication of the NIH ARDS Network study.(15, 60) However, some patients remain at risk for overdistention injury even when small  $V_T$ s are used because their aerated lung volumes are greatly reduced.(20, 25) As PBW does not correlate well with aerated lung volume, better approaches to setting  $V_T$  may involve limiting lung stress, strain, or driving pressure, as potential surrogates for VILI from parenchymal overdistention injury. Whatever method is initially utilized, for patients with moderate-severe ARDS or more severely impaired respiratory mechanics, we suggest the

careful, continued further reduction of  $V_T$  in a stepwise manner until a patient begins to exhibit physiologic signs of intolerance or the DP or Pplat is in a safer range. (Table 1) As is frequently the case, this intervention will have competing effects that must be balanced on a patient-by-patient basis. Higher levels of PEEP may be necessary to prevent atelectasis that may result from the smaller  $V_T$ s. However, higher PEEP may cause overdistention or hemodynamic instability.(61) The need for strict control of PaCO<sub>2</sub>, as in intracranial hypertension, may outweigh the need to lower  $V_T$  to protect the lung. Nevertheless, we recommend keeping  $V_T$  at the lowest possible value as dictated by patient tolerance and appropriateness of respiratory mechanics, gas exchange, and hemodynamic parameters. As the technology of ECCO<sub>2</sub>R continues to evolve, the limits of MV with low  $V_T$ s as a lung protective strategy should continue to be tested. Further investigations are warranted to determine if pushing the limits of lowering  $V_T$  will improve clinical outcomes.

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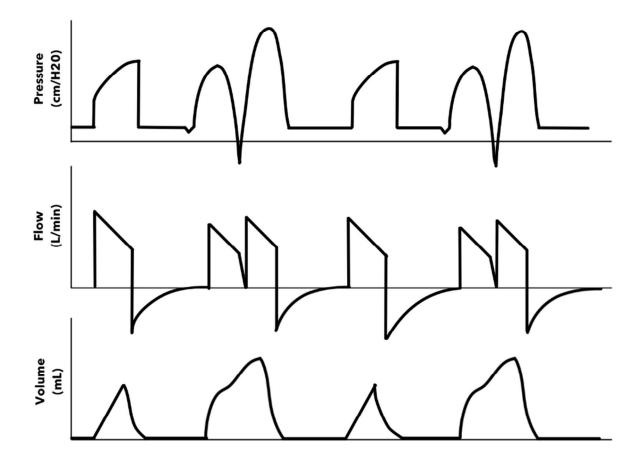


Figure 1: Patient-ventilator dyssynchrony with triggering of double breaths from the ventilator in Volume-Assist control mode. The first channel demonstrates airway pressure with a normal breath followed by a double breath triggered by the patient. The second channel shows flow during a normal breath followed by a double breath. Patient inspiratory effort continues beyond the set ventilator inspiratory time, resulting in airway pressure decreasing below the PEEP and triggering a second breath during the same patient effort. This may result in high lung pressures (during the double breath – panel 1) and high volumes. The third channel demonstrates increased volumes during double triggered breaths. If patients consistently trigger double breaths, they will not be receiving low tidal volumes for lung protection during the double breath and are at increased risk for volutrauma.

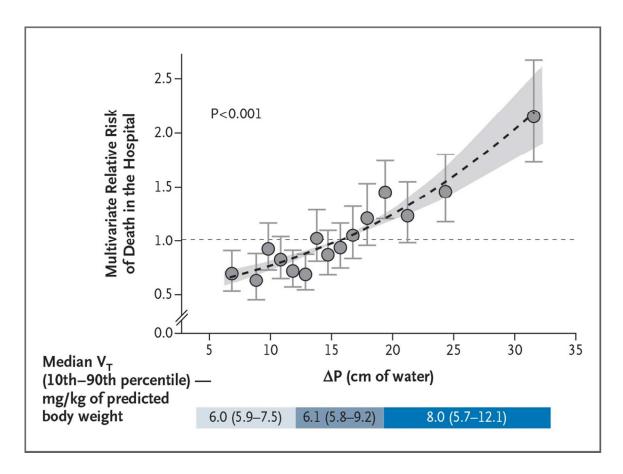


Figure 2: Driving pressure versus adjusted relative risk of death

Relative Risk of Death in the Hospital versus Driving Pressure in the Combined Cohort after Multivariate Adjustment. Even below the median driving pressure of 14 cm H<sub>2</sub>O, there is still a significant risk of death in the hospital. Amato MBP et al. N Engl J Med 2015;372:747-755. (32) Reprinted with permission.

Table 1: Signs of intolerance to low V<sub>T</sub> and hypercapnia

Signs of Low V <sub>T</sub> Intolerance
Tachycardia
Hypertension
Hypotension
Tachypnea
Patient – ventilator dyssynchrony, e.g. double
triggering
Inspiratory airway pressure below PEEP, indicating
high work of breathing
Respiratory Acidosis
Hypoxemia despite high FiO2
Agitation

Table 1: Physiologic signs that can be assessed for evidence of intolerance to mechanical ventilation with low  $V_T$ s and hypercapnia. Patient-ventilator dyssynchrony often manifests as a double breath (see Figure 1) which means the end-inspiratory pressure and end-inspiratory lung volume are higher than at the end of synchronous breath, which is a major risk for alveolar overdistention.